AMENDMENTS TO THE SPECIFICATION:

Please replace the paragraph that begins on page 4, line 17 with the following paragraph:

> In accordance with a further aspect of the present invention, a method of manufacturing a stent coating is disclosed including applying a composition to a stent, the composition including a semicrystalline polymer and a solvent; allowing the solvent to evaporate to form a dry coating, the dry coating comprising less than about 2% residual fluid content (w/w); and exposing the coating to a fluid for a sufficient duration to increase the crystallinity of the polymer in at least a portion of the coating, the fluid being substantially free from any polymer. In one embodiment, the polymer comprises an ethylene vinyl alcohol copolymer or poly(vinylidene fluoride-co-hexafluoro[[r]]propene). In another embodiment, exposing the coating to a fluid includes immersing the stent into a bath of fluid. In yet another embodiment, the stent is immersed for about 30 minutes to about twelve hours.

Please replace the paragraph that begins on page 13, line 14 with the following paragraph:

> "Percent crystallinity" refers to the percentage of the polymer material that is in a crystalline form. In one embodiment of the present invention, the polymer is a semicrystalline polymer having between 10 and 75 percent crystallinity. For example, poly(vinylidene fluoride-co-~~hexafluroisopropylene~~hexafluoroisopropylene) can achieve about 20% crystallinity when the vinylidene fluoride to ~~hexafluroisopropylene~~ hexafluoroisopropylene ratio is 85:15. Also, by example, poly(vinylidene fluoride) can achieve about a 65 percent crystallinity, and poly(6-aminocaproic acid) can achieve about a 64 percent crystallinity.

Please replace the paragraph that begins on page 17, line 1 with the following paragraph:

The fluid treatment process parameters are selected to limit the penetration of the fluid into the thickness of the coating. By limiting the treatment process, a coating can be produced in which the shallower regions of the coating have a different coating morphology than the deeper regions. For example, a volatile fluid (e.g., acetone) or a limited process duration can be used so that most of the fluid is evaporated before penetrating into the deep regions of the coating. One of ordinary skill in the art will understand that the fluids cho[[o]]sen or the duration of the fluid treatment will depend on factors such as the desired diffusion rate of the active agent through the polymer, and the inherent characteristics of the polymers and active agents used in the coating.

Please replace the paragraph that begins on page 21, line 22 with the following paragraph:

One can account for the foregoing factors by using a test polymer that is substantially the same as the coating polymer, and is tested under substantially the same conditions as the conditions used to conduct the fluid treatment of the polymeric coating. The test polymer should have the same chemical structure as the coating polymer, and should have substantially the same molecular weight and molecular-weight distribution as the coating polymer. For example, if the polymer is a blend of copolymers or homopolymers, the test polymer should have substantially the same percentage of components as the coating polymer. At the same time, the test polymer should have substantially the same crystallinity as the coating polymer. Methods of determining ~~crystallinity~~ crystallinity are discussed herein. Additionally, the composition used to form the test polymer should include the same compounds (e.g., additives such as therapeutic substances) and liquids (e.g., solvent(s) and water) that are mixed with the coating polymer. Moreover, the test polymer should have the same thermal history as the coating polymer. The test polymer should be prepared under the same conditions as the coating polymer, such as using the same solvent, temperature, humidity and mixing conditions. Finally, the heating rate used for measuring the transition temperature of the test polymer should be substantially similar to the heating rate used to conduct the fluid treatment of the polymeric coating.

Please replace the paragraph that begins on page 29, line 3 with the following paragraph:

> As noted above, "polymer" as used herein is inclusive of homopolymers, copolymers, terpolymers etc., including random, alternating, block, cross-linked, blends and graft variations thereof. By using the methods of measurement described above, one may observe more than one T_g for some of these types of polymers. For example, some polymer blends that exhibit two phase systems can have more than one T_g. Additionally, some semicrystalline polymers can have two glass transitions, especially when they have a higher percent crystallinity. See Edith A. Turi, ~~Theraml~~ Thermal Characterization of Polymeric Materials, Academic Press, Orlando, FL (1981). Bulk-crystallized polyethylene and polypropylene, for example, can have two glass transition temperatures at a relatively high percent crystallinity. The lower of the two transitions is represented as $T_g(L)$, which can be the same as the conventional T_g at zero crystallinity. The higher transition is designated as $T_g(U)$ and becomes more detectable as the crystallinity increases. The difference, $\Delta T_g = T_g(U) - T_g(L)$, tends to approach zero as the fractional ~~crystallnity~~ crystallinity χ approaches zero.

Please replace the paragraph that begins on page 35, line 10 with the following paragraph:

> Representative examples of polymers that can be combined with the active agent for the reservoir layer include ethylene vinyl alcohol copolymer (commonly known by the generic name EVOH or by the trade name EVAL); polybutylmethacrylate; poly(ethylene-co-vinyl acetate); poly(vinylidene fluoride-co-hexafluoro[[r]]propene); poly(hydroxyvalerate); poly(L-lactic acid); poly(epsilon-caprolactone); poly(lactide-co-glycolide); poly(hydroxybutyrate); poly(hydroxybutyrate-co-valerate); polydioxanone; polyorthoester; polyanhydride; poly(glycolic acid); poly(D,L-lactic acid); poly(glycolic acid-co-trimethylene carbonate); polyphosphoester; polyphosphoester urethane; poly(amino acids); cyanoacrylates; poly(trimethylene carbonate); poly(iminocarbonate); copoly(ether-esters) (e.g. PEO/PLA); polyalkylene oxalates;

polyphosphazenes; biomolecules, such as fibrin, fibrinogen, cellulose, starch, collagen and hyaluronic acid; polyurethanes; silicones; polyesters; polyolefins; polyisobutylene and ethylene-alphaolefin copolymers; acrylic polymers and copolymers; vinyl halide polymers and copolymers, such as polyvinyl chloride; polyvinyl ethers, such as polyvinyl methyl ether; polyvinylidene halides, such as polyvinylidene fluoride and polyvinylidene chloride; polyacrylonitrile; polyvinyl ketones; polyvinyl aromatics, such as polystyrene; polyvinyl esters, such as polyvinyl acetate; copolymers of vinyl monomers with each other and olefins, such as ethylene-methyl methacrylate copolymers, acrylonitrile-styrene copolymers, ABS resins, and ethylene-vinyl acetate copolymers; polyamides, such as Nylon 66 and polycaprolactam; alkyd resins; polycarbonates; polyoxymethylenes; polyimides; polyethers; epoxy resins; polyurethanes; rayon; rayon-triacetate; cellulose acetate; cellulose butyrate; cellulose acetate butyrate; cellophane; cellulose nitrate; cellulose propionate; cellulose ethers; and carboxymethyl cellulose.

Please replace the paragraph that begins on page 55, line 2 with the following paragraph:

The following experiment was conducted in order to obtain information on how the fluid treatment process could affect polymer morphology. Pellets of poly(vinylidene fluoride-co-hexafluoro[[r]]propene) (SOLEF 21508, available from Solvay Solexis PVDF, Thorofare, NJ) were placed in a sealable container. The treatment fluid, ethyl acetate, was added to the container at a 1:7 polymer:fluid ratio (w/w) and the container was sealed. The contents of the container were agitated at room temperature for about five hours by using a magnetic stir bar. Upon visible inspection, the pellets about doubled in size, indicating that the fluid caused the polymer to swell. After the treatment, the polymer pellets were removed from the container and dried at 50°C overnight.

Please replace the paragraph that begins on page 55, line 12 with the following paragraph:

A Fourier Transform Infrared (FTIR) analysis was conducted on a control group (i.e., pellets of poly(vinylidene fluoride-co-hexafluoro[[r]]propene) which had not been exposed to the fluid treatment). The results for the control group are illustrated in the spectrograph of Figure 5A. An FTIR analysis was also conducted on the pellets exposed to the fluid treatment. The results for the fluid treatment group are illustrated in the spectrograph of Figure 5B. The spectra of Figures 5A and 5B are substantially similar, except that a peak near 975 cm^{-1} appears for the polymer treated with the fluid as shown in Figure 5B.

Please replace the paragraph that begins on page 56, line 5 with the following paragraph:

18 mm VISION stents (available from Guidant Corporation) are coated by spraying a 2% (w/w) solution of poly(vinylidene fluoride-co-hexafluoro[[r]]propene) (~~e.g.,~~ e.g., SOLEF 21508) and 40-O-(2-hydroxy)ethyl-rapamycin mixed with a solvent having 30:70 acetone/cyclohexanone (w/w). The drug to polymer ratio for the coating is 1.25 to 1. The target drug loading is 160 μg. The solvent is removed by baking at 50°C for 2 hours to produce a dry drug coating. Next, the stents are immersed in a hydrofluoroether solvent (e.g., NOVEC HFE7200, ethoxy-~~nonaflurobutane~~nonafluorobutane ($C_4F_9OC_2H_5$), available from 3M, St. Paul, MN) for five minutes for a fluid treatment. The stents are then removed from the hydrofluoroether solvent and baked to remove essentially all of the fluid.